

Electromagnetic Design of flexIble SensOrs



Report 96 CISS for zeros-poles, error

dr eng. Grzegorz Fotyga July 12, 2021





European Union European Regional Development Fund



"EDISOn–Electromagnetic Design of flexIble SensOrs" Project, Agreement POIR.04.00-00-1DC3/16-00 date December 6, 2016, within the TEAM-TECH Program of the Foundation for Polish Science co-financed by the European Union under the European Regional Development Fund.



Figure 1: Bandpass filter.



Figure 2: S - characteristics (ROM).

1 Test Structure

- Bandpass filter.
- Poles and zeros are extracted from the eigenproblem associated with reduced order model.

2 Eigenproblem

Model order reduction system of equations (S-params formulations):

$$\begin{cases} (\mathbf{T}_r - k_0^2 \mathbf{C}_r + ik_0 c\epsilon_0 (\mathbf{B}_r d) \cdot (\mathbf{B}_r d)^T) \cdot \mathbf{x}_r = 2\mathbf{b}_r^j da \\ b = ik_0 c\epsilon_0 (\mathbf{b}_r^j d)^T \mathbf{x}_r - a \end{cases}$$
(1)

which can be transformed to the matrix form (assuming b = 0):

$$\begin{pmatrix} \begin{bmatrix} \mathbf{T}_r & -2\mathbf{b}_r^j d \\ 0 & -\delta_{ij} \end{bmatrix} + k_0 \begin{bmatrix} ic\epsilon_0(\mathbf{B}_r d) \cdot (\mathbf{B}_r d)^T & 0 \\ ic\epsilon_0(\mathbf{b}_r^i d)^T & 0 \end{bmatrix} + k_0^2 \begin{bmatrix} -\mathbf{C}_r & 0 \\ 0 & 0 \end{bmatrix} \end{pmatrix} \begin{bmatrix} \mathbf{x}_r \\ a \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

The above eigenproblem is solved using CISS in order to compute **transmission and reflection zeros** of the scattering parameters. **Poles** are computed by solving the eigenproblem:

$$(\mathbf{T}_r - k_0^2 \mathbf{C}_r + ik_0 c\epsilon_0 (\mathbf{B}_r d) \cdot (\mathbf{B}_r d)^T) \cdot \mathbf{x}_r = 0$$
⁽²⁾



Figure 3: S11 - characteristics (ROM/zeros-poles from band: 3-10GHz).



Figure 4: S11 - characteristic obtained using ROM and the error ϵ computed using (3).

3 S-characteristics obtained using zeros-poles compared to the original ones

The plot below (Fig.3) shows S11 characteristic based on the FEM MOR approach and characteristic S_{11}^{ZP} obtained using zeros-poles from the band 3-10GHz:

$$S_{11}^{ZP} = 20 \log_{10} \left(\left| \frac{(s-z_1) \cdot (s-z_2) \cdot \dots \cdot (s-z_n)}{(s-p_1) \cdot (s-p_2) \cdot \dots \cdot (s-p_m)} \right| \right)$$
(3)

 $\bullet \ s=j\omega$

- n is the number of zeros in the band 3 10 GHz
- m is the number of poles in the band 3 10 GHz
- z are zeres from band 3 10GHz
- p are poles from band 3 10 GHz

4 Error

The next plot (Fig.4) show the same S11 characteristic together with the error ϵ :

$$\epsilon = 20 \log_{10} \left(\left| \frac{(s-z_1) \cdot (s-z_2) \cdot \dots \cdot (s-z_n)}{(s-p_1) \cdot (s-p_2) \cdot \dots \cdot (s-p_m)} \right| - \left| \frac{(s-\tilde{z}_1) \cdot (s-\tilde{z}_2) \cdot \dots \cdot (s-\tilde{z}_k)}{(s-\tilde{p}_1) \cdot (s-\tilde{p}_2) \cdot \dots \cdot (s-\tilde{p}_l)} \right| \right)$$
(4)

where:

- $s = j\omega$
- n is the number of zeros in the band 3 10 GHz
- m is the number of poles in the band 3 10 GHz
- k is the number of zeros in the band 4 6GHz
- l is the number of poles in the band 4 6GHz
- z and \tilde{z} are zeros from band 3 10GHz and sub-band 4 6GHz, respectively
- p and \tilde{p} are poles from band 3 10 GHz and sub-band 4 6 GHz, respectively